

## Electrical behavior of graphite epoxy composite electrodes in humid environment

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Received: March 10, 2023; Revised: April 20, 2023

The present study demonstrates the development of graphite (GR)-enriched epoxy composites for possible application as electrode materials for supercapacitors operating in humid environment. The study was conducted through development of a series of adhesive compositions involving epoxy resin supplemented with various proportions of GR (50 to 85 %w/w) and 4,4'-diaminodiphenyl sulfone (1%, w/w), followed by curing over stainless-steel current collectors at 110 °C. This has afforded a series of working electrodes (WEs) with improved electrical conductivity. The effect of temperature and voltage on the electrical behavior of WEs at varying composition was investigated in humid environment (40%, RH). The study demonstrates that WEs involving 50 wt% of GR exhibit a 10% increase in  $\sigma_{DC}$  at 1 V under 40% RH, 40°C. Arrhenius plots revealed that the activation energies ( $E_a$ , J/mole) of WEs were dependent on GR concentration (50 to 75% w/w) and were found in the range of 2.10 to 4.76. In comparison to the humidity at room temperature (36% RH), the humidity exposure (40% RH) of WEs derived at 50 wt% GR has shown an increase in  $\sigma_{DC}$  by 7.69%.

**Keywords:** Humidity, Epoxy, Graphite, Electrical conductivity, Working electrodes

### INTRODUCTION

The current century has witnessed a growing need of inexpensive electronic materials for microelectronics [1], energy conservation and storage [2-4]. Working electrodes (WEs) constitute a crucial component in portable electronic devices, including batteries and supercapacitors pertaining to power generation and charge storage. The exploration of renewable and energy-efficient WEs for batteries and supercapacitors relies on the utilization of electrically conducting and electroactive materials possessing commendable temperature, voltage regulated conducting behavior [1], sustainability in humid environment [5] and ease of fabrication [6]. The adequate performance of WEs necessitates their high heat resistance and stability in humid conditions. In this regard, electrically conducting WEs with stability up to 200°C were developed from polyindole in presence of tungsten carbide [7]. Another study demonstrated an enhancement in the semiconducting behaviour of polypyrrole by incorporating haemoglobin [4]. A study reported that supercritical CO<sub>2</sub> assisted the green method for the synthesis of composite with improved DC conductivity and thermal stability [3]. In a recent study, thermally stable WEs (1000°C) were derived from carboxylate functional multi walled carbon nano tubes (MWCNTs) in presence of hexagonal boron nitride and polyvinyl butyral.

The study reveals an increase in  $\sigma_{DC}$  ranging from 0.96 to 1.14 under humidity exposure (40%) up to 3 h. However, further humidity exposure up to 9 h has marginally declined the  $\sigma_{DC}$  from 1.11 to 1.10 under identical conditions [8].

Graphite is widely known as an electrically conducting filler for polymer materials, especially epoxy resin to afford the polymer composites for electronic and electrochemical applications. Over decades, considerable progress has been noticed in development of polymer nanocomposites through reinforcing various allotropic variants of graphite with epoxy resins. The key allotropic variants used in the development of electrically conducting polymer nanocomposites involving epoxies are expanded graphite, graphite [10, 11], graphite nanoparticles [12, 13] and carbon black [14]. A study involving expanded graphite (8 wt %) reveals an 11-fold increase in  $\sigma_{DC}$  of epoxy [9]. However, graphite as a filler poorly contributes to  $\sigma_{DC}$  of epoxy composite, as reported [10, 11].

Reinforcing graphite by 5 to 25 % contributes to the  $\sigma_{DC}$  ( $\times 10^{-6}$ ) S/cm ranging from 2.5 to 3.39 [10]. In another study the increase in graphite loading up to 55 wt% imparts the  $\sigma_{DC}$  of epoxy composite in the order of  $10^{-4}$  S/cm [11]. Reinforcing graphite nano particles (0.3 to 30 wt %) into epoxy imparts  $\sigma_{DC}$  of polymer composite by the order of  $10^{-3}$  S/cm [12].

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Although a wide range of allotropic variants of graphite has been investigated to develop the electrically conducting epoxy composites and their nano composite analogues, no efforts are yet reported on the investigation of their electrical behaviour in humid environment.

Epoxy is widely used as an insulating material, and its response to elevated humidity levels has been extensively studied [15-22]. Epoxy/epoxy compounds in humid environment can undergo dimensional changes [13-15], reduction in mechanical properties [16, 17], increased susceptibility to environmental stress cracking [19, 20] and altered thermal properties [23, 24]. Epoxy resins have shown different mechanisms of water absorption *via* hydrogen bonding under different RH exposure based on their structure and activation energies [25, 26]. In a study it was found that addition of MWCNTs (1 wt%) to epoxy resulted in moisture uptake similar to cured epoxy, however, reduction in diffusivity was observed [16]. The dependence of  $\sigma_{DC}$  of GR/epoxy composites on RH has not been extensively studied. The present study investigates the humidity and temperature dependence of electrical conductivity of epoxy GR composites at varying voltage.

## EXPERIMENTAL

### *Materials and methods*

Working electrodes (WEs) were fabricated using commercially available GR powder (purity 98%, surface area 250  $\mu\text{m}$ ) sourced from Loba Chemie Fine Chemicals Pvt. Ltd, India. Epoxy (CY-230, density 1.08 g/cc) and hardener (4,4'-diaminodiphenyl sulfone, HT-972) were obtained from Huntsman India Pvt Limited. Other chemicals and solvents (>99%) were locally arranged and used without further purification.

### *Fabrication of working electrodes*

A series of WEs were fabricated through curing of an adhesive composition involving epoxy resin supplemented with various proportions of GR in acetone medium over stainless steel current collectors (CC). The CC employed for development of WEs were of 1  $\text{cm}^2$  area and a thickness of  $1.48 \pm 0.01$  mm. A representative procedure involving the adhesive composition of epoxy resin (CY-230) with GR (50 to 85 w/w%) was thoroughly mixed at 800 rpm, followed by thermal activation at  $90^\circ\text{C} \pm 1^\circ\text{C}$  for 1 h and curing over CC with 4,4'-diaminodiphenyl sulfone (1%, w/w) at  $50^\circ\text{C} \pm 1^\circ\text{C}$ . Prior to curing, the surface of CC was polished with emery paper and subsequently cleaned with acetone. WEs were post-cured at  $110^\circ\text{C}$ . WEs with GR (% w/w) 0, 50, 65, 75

and 85 were fabricated and abbreviated as WE-0, WE-I, WE-II, WE-III and WE-IV, respectively. WEs with coating thickness of  $0.23 \pm 0.01$  mm were isolated and stored at  $50 \pm 1^\circ\text{C}/400$  mm Hg [27]. The morphology of the electrode surface was examined through gold sputtering on its surface followed by scanning electron microscopy (SEM) imaging on JEOL JSM-6610 LV at 15 kV.

### *DC conductivity measurement*

DC conductivity ( $\sigma_{DC}$ ) measurements were conducted at  $25 \pm 1^\circ\text{C}$  using a four-probe setup equipped with Keithley nanovoltmeter 2182A and a 6221 DC current source. The activation energy ( $E_a$ , J/mol) of the WEs was calculated within the temperature (K) range of 313.15 to 373.15 according to the Arrhenius equation  $\sigma_{DC} = \sigma_0 DC \exp(-E_a/K_B T)$ , where  $\sigma_{DC}$  is electrical conductivity ( $\mu\text{S}/\text{cm}$ ) of WEs,  $E_a$  is activation energy (eV) which indicates the energy needed for an electron to skip and move to adjacent vacancy,  $\sigma_0 DC$  is pre-exponential factor which corresponds to maximum electrical conductivity (that it would have at infinite temperature),  $T$  is absolute temperature, and  $K_B$  is Boltzmann's constant [28-30]. Oven-dried electrodes were aged in humid environment. Relative increase in  $\sigma_{DC}$  of WEs under humidity exposure at 36% and 40% were investigated at selected voltages over the interval of 1 h till 8 h at  $40 \pm 1^\circ\text{C}$ .

## RESULTS AND DISCUSSION

### *Microstructure*

Dispersion of GR into epoxy matrix of WEs was revealed through SEM (Figure 2). Dispersion of GR into epoxy has been associated with occasional phase separation in the epoxy matrix. The bright and dark phases associated demonstrate the epoxy- and GR-rich phases of WEs. Early studies revealed saturation of the epoxy matrix with 55 wt% of GR cured with aliphatic amine hardener without significant phase separation [11]. In the present investigation, WEs derived through dispersion of 50 to 85 wt% of GR revealed phase separation at 1KX, 10  $\mu\text{m}$ , due to the insoluble nature of the solid phase hardener (HT-972) into epoxy resin (Figure 2b). The concerned phase separation was well distinct at 3KX, 5  $\mu\text{m}$  indicating the dispersion of graphene layers derived from GR into epoxy matrix.

In a study on GR/epoxy it was reported that at the elevated temperature employed during the curing process of epoxy, the viscosity of epoxy resin diminished, thereby enhancing the mobilization of the filler phase within the polymer phase. This increased the affinity of the filler to engage with the

matrix and establish conductive filler networks [31]. On further increase in GR concentration in epoxy (85%), the WE-IV resulted in dense clusters of graphene layers into the epoxy matrix (Figure 2d). WE-IV at 1KX, 10  $\mu\text{m}$  revealed a saturation of the graphene layers within the epoxy matrix, displaying a significant presence of clusters formed by epoxy-bonded GR (Figure 2b). Another study revealed that reinforcement of GR (80 wt.%) results in decreased processability due to high viscosity. In the current investigation, the loading of 85 wt% of GR was found to adequately bind with epoxy matrix while preserving a phase-separated morphology over WEs (Figure 2d) [32].

#### Electrical behavior

Figure 2 reveals the trend of  $\sigma_{\text{DC}}$  of WEs (36% RH) with concentration of GR (wt%) at selected voltages at  $25 \pm 1^\circ\text{C}$ . In general,  $\sigma_{\text{DC}}$  of WEs increased with GR concentration (wt%) and voltage. The increase in  $\sigma_{\text{DC}}$  of WEs with GR concentration

attributes to long-range conductive interconnections between the filler and the epoxy matrix. This observation is supported by the early reports of  $\sigma_{\text{DC}}$  on the close agreement with  $\sigma_{\text{DC}}$  epoxy nanocomposites involving MWCNT and GR [11, 33]. However, the relative difference in  $\sigma_{\text{DC}}$  for individual WEs was marginal at 1V and 10V. These observations revealed the electrically insulating behaviour of WEs up to 10V. This observation was in close agreement with epoxy nanocomposites prepared out of expanded graphite [9]. Present observations indicated that WE-IV with 85 wt% reinforcement of GR imparts enhanced  $\sigma_{\text{DC}}$  (859.80  $\mu\text{S}/\text{cm}$ ) at 100V over the epoxy composite (100  $\mu\text{S}/\text{cm}$ ) involving expanded graphite (8 wt%) at 1000 V. Moreover, an increase in voltage from 1 V to 100 V has raised the  $\sigma_{\text{DC}}$  of WE-IV 11 times over WE-0 [34]. Dispersion of carbonaceous fillers plays constructive role towards enhancing the electrical behavior of epoxy composites [35].

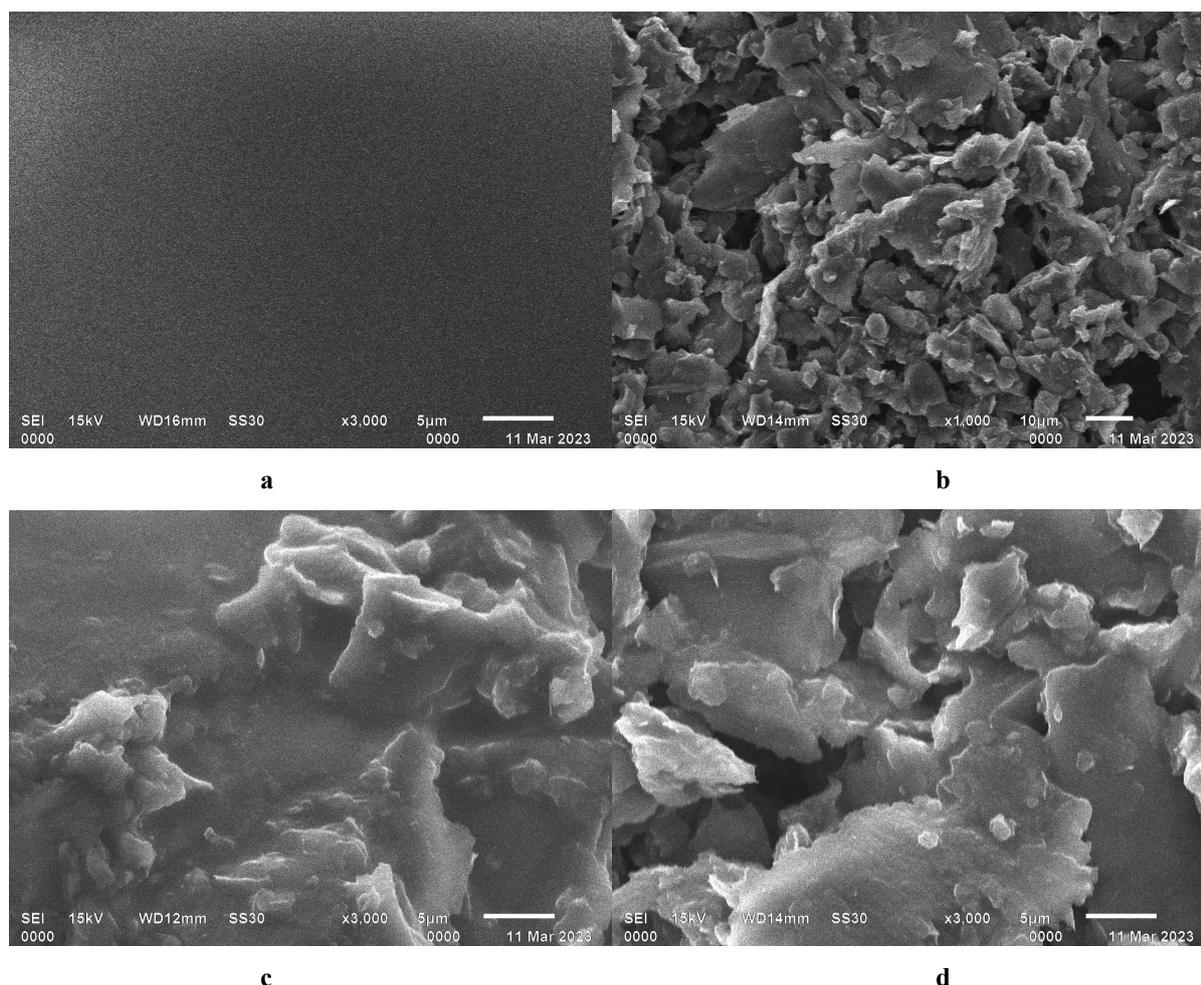


Fig. 1. SEM of WE-0 (a) and WE-IV (b) at 1KX, 10  $\mu\text{m}$ , WE-I(c) and WE-IV(d) at 3KX, 5  $\mu\text{m}$

In the present investigation the exceptionally enhanced  $\sigma_{DC}$  (859.80  $\mu\text{S}/\text{cm}$ ) of WE-IV at 100 V was supported by SEM which indicates the prominent dispersion of graphene layers (bright phase) into epoxy matrix (dark phase) (Figure 1c).

Figure 3. demonstrates the linear I-V characteristics of WEs at  $25 \pm 1^\circ\text{C}$ . The ohmic behavior of WEs appeared in the range of 0.10 to 2.08  $\mu\text{A}$  with corresponding voltage ranging from 20 to 55 V [36]. Table 1 shows the increase in  $\sigma_{DC}$  of WEs with varying voltage (1V–100V) and temperature ranging from 293 to 393 K. Figure 4 illustrates a decline in  $\sigma_{DC}$  of WE-IV with temperature (K) ranging from 333 to 393 at 100 V. This consistent trend attributes to the enhancement in the collaborative motion of the macromolecular segments of epoxy, triggered with temperature elevation. This movement leads to a greater dissipation of energy, thereby contributing to the observed decrease in  $\sigma_{DC}$  [37]. Using the theoretical Arrhenius model, the calculated activation energies from plots of  $\log(\sigma_{DC})$  against  $1000/T$  at 100 V revealed  $E_a$  (J/mol) for WEs in the sequence of WE-0 (4.19), WE-I (2.10), WE-II (3.97), WE-III (4.76) (Figure 5).

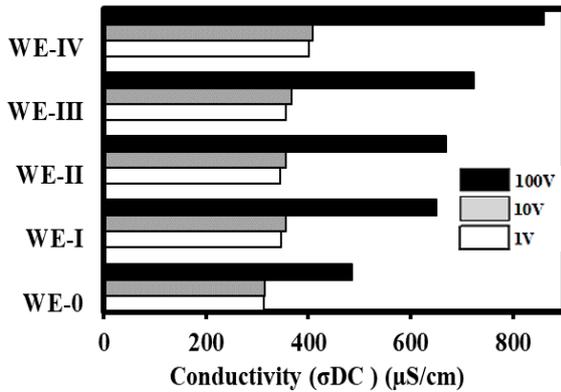


Fig. 2. Effect of voltage on  $\sigma_{DC}$  ( $\mu\text{S}/\text{cm}$ ) of WEs

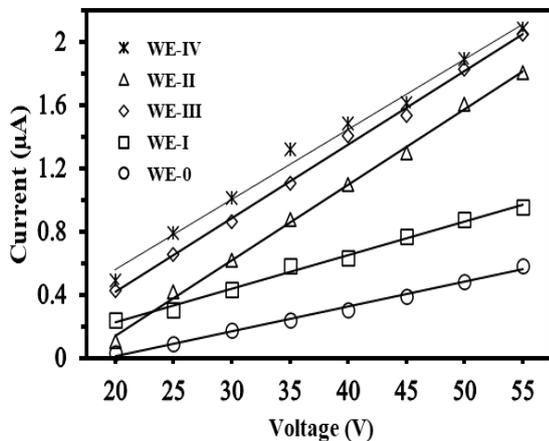


Fig. 3. Ohmic behavior of WEs

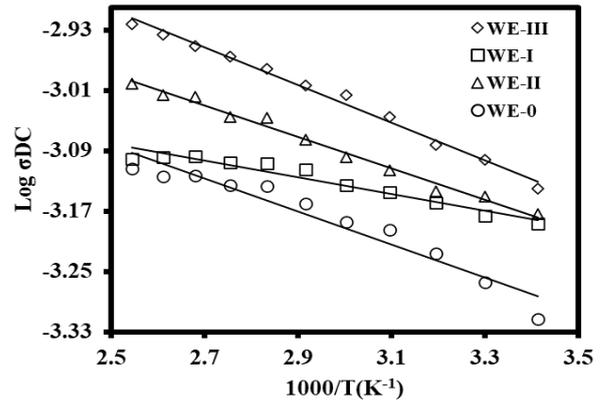


Fig. 4. Arrhenius plots of the DC conductivity for WEs

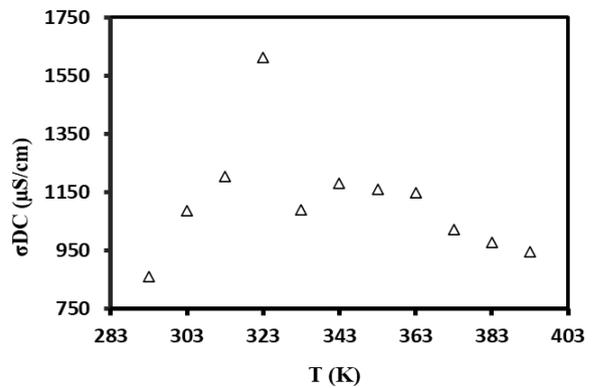


Fig. 5. Effect of temperature on  $\sigma_{DC}$  ( $\mu\text{S}/\text{cm}$ ) of WE-IV at 100 V

#### Effect of humidity

WEs were developed at selected wt% of GR and investigated for the electrical behavior after 8 h of exposure at 40% RH%. In general, the  $\sigma_{DC}$  ( $\mu\text{S}/\text{cm}$ ) of WEs was dependent on their composition. Figure 6 demonstrates the effect of wt% of GR and voltage (V) on  $\sigma_{DC}$  of WEs. The  $\sigma_{DC}$  of WE-I was increased by 10.30% at 1 V and by 7.55% at 100 V. WE-II has shown an increase in  $\sigma_{DC}$  by 5.23 % at 1 V. However, at 100 V, WE-II has shown an increase of  $\sigma_{DC}$  by 1.44 % .The rest of the WEs has shown a significant decrease in their  $\sigma_{DC}$  ( $\mu\text{S}/\text{cm}$ ) ranging from 859.39 to 822.2. Duration of humidity on WEs based on GR oxide/epoxy revealed an increase in their  $\sigma_{DC}$  from  $10^{-6}$  to  $10^{-2}$  S/cm when RH was increased from 30% to 100% [5]. Epoxy resins cured with amines are associated with inherent hygroscopic nature due to the formation of hydroxyl group in their macromolecular segment [8, 15]. A study on carbon/epoxy composites has reported that the presence of carbonaceous fillers reduced the moisture-absorbing capacity of the composite by 3% [38]. For such reasons, WE-I, WE-II developed at higher proportion of epoxy absorbed the moisture to a great extent over those prepared at low proportion of epoxy (WE-III, WE-IV).

A detailed insight into the effect of humidity on  $\sigma_{DC}$  of WEs and their electrical behavior was obtained at competitive RH% selected at 36 and 40 (Figure 7). The increase in RH from 36 to 40, has raised the  $\sigma_{DC}$  of WE-I from 650 to 700 at 100 V. The calculations revealed that the increase in RH by 4% imparts 7.69% increase in  $\sigma_{DC}$  of WE-I at 100 V. However, subsequent WEs were found resistant towards humidity and have not contributed to further increase in their  $\sigma_{DC}$  under the differential exposure of RH by 4% at 100 V. The present investigation is in agreement with the literary report that reveals insulating properties of graphene oxide thin films at low RH. Presence of epoxy contributes to the ion conducting mechanism within the polymer matrix that causes an increase in  $\sigma_{DC}$  of WEs [39]. However, with increase in % GR, the relative proportion of epoxy decreased, that delivers the WEs, wherein the  $\sigma_{DC}$  is insignificantly increased, thus leaving WEs with intact electrical behavior.

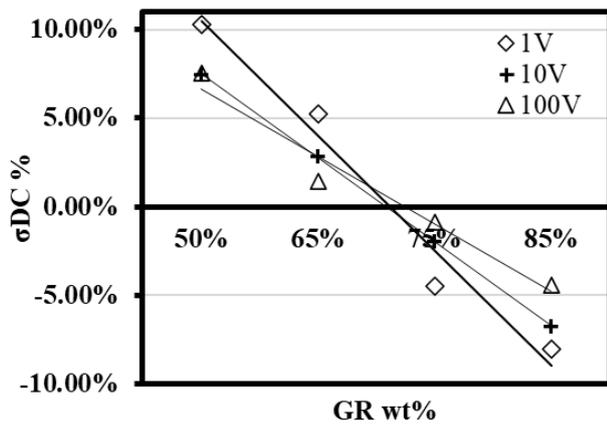


Fig. 6. Effect of composition and voltage on  $\sigma_{DC}$  of WEs at RH (40%)

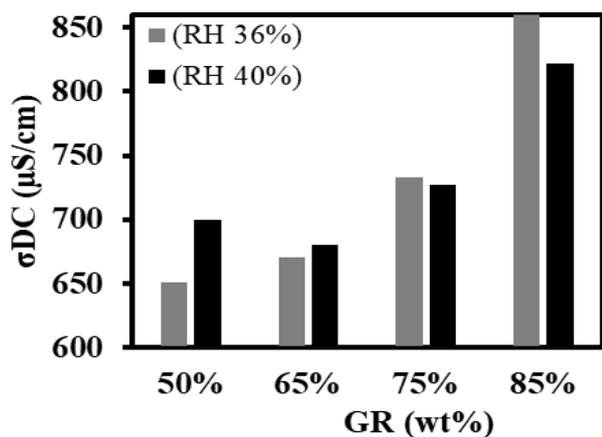


Fig. 7. Effect of composition and RH % on  $\sigma_{DC}$  of WEs.

Table 1. Effect of temperature on the conductivity of WEs at 100V

T(K)	WE-0	WE-I	WE-II	WE-III	WE-IV
393	486.35	650.95	670.24	743.54	946.71
383	543.97	667.41	707.84	791.04	977.17
373	594.69	694.72	717.84	826.94	1023.29
363	639.38	716.35	765.46	901.34	1024.20
353	654.49	733.11	797.00	963.84	1082.01
343	691.67	768.37	842.29	992.35	1092.13
333	729.38	783.39	899.00	1043.77	1389.70
323	732.77	784.14	902.77	1084.25	1612.37
313	754.89	800.25	958.71	1119.85	1319.50
303	751.18	796.64	963.08	1160.35	1096.13
293	771.11	792.29	998.98	1197.09	859.88

### CONCLUSIONS

Working electrodes (WEs) based on epoxy supplemented with graphite (GR) (wt% 50 to 85) were developed *via* curing process on a stainless-steel current collector. The developed WEs revealed saturation at 85 wt% GR which showed clear phase separation and dense clusters of graphene layers within the epoxy matrix. With GR wt% the  $\sigma_{DC}$  ( $\mu S/cm$ ) of WEs was found to increase by 859.80 for WE-IV at 100V, 36% RH and  $25 \pm 1^\circ C$ . The study demonstrated an 11-fold increase in  $\sigma_{DC}$  of WE-IV over WE-0 at variable voltage ranging from 1 V to 100 V. The present investigation suggests that dispersion of carbonaceous fillers plays a constructive role towards enhancing the electrical behaviour of epoxy composites. The study also demonstrated that with the rise in temperature from 293 to 393 K and varying voltage (1 V–100 V) the WEs exhibited an increase in  $\sigma_{DC}$  with temperature. A detailed investigation on the effect of humidity on  $\sigma_{DC}$  of WEs revealed that  $\sigma_{DC}$  is greatly influenced by changes in relative humidity. WEs under differential exposure of RH by 4% at 100V showed an increase of 7.69 % in  $\sigma_{DC}$  of WE-I, however, other electrodes were insignificantly affected. The WE-I at 40% RH showed an increase in  $\sigma_{DC}$  by 10.30 % at 1 V and 7.55 % at 100 V. The present study demonstrates that the presence of relatively higher wt% of epoxy in WE-I, II, has significantly contributed to increased  $\sigma_{DC}$  owing to its hygroscopic nature and hydroxyl groups.

**Acknowledgement:** Authors are grateful to Defence Research Development Organization, Ministry of Defence, India, for financial support vide grant No CFEES/TCP/EnSG/CARS/Pantnagar/ MOFW/20 /2018 for development of experimental facilities at Pantnagar.

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